

## Homework #4 Solutions

2. (a) In equilibrium,  $C_{B_3I} = K(C_{B^-})^3 C_{I^0} \left(\frac{p}{n_i}\right)^3$

where  $K = \frac{1}{(C_s)^3} \exp\left(\frac{\Delta G_{\text{binding}}}{kT}\right)$

Since we use  $\left(\frac{p}{n_i}\right)$ ,  $\Delta G_{\text{binding}}$  is defined for  $n=p=n_i$ .  
 (could use any reference, e.g.  $p=N_v$  for  $E_f = E_v$ )  
 If  $p > n_i$ , the reference hole energy is higher, so binding energy is larger.

@ 900°C,  $n_i = 3.2 \times 10^{18} \text{ cm}^{-3}$ ,  $C_{I^0} = 4.8 \times 10^{10} \text{ cm}^{-3}$ .  $C_{B^-} \gg n_i$ , so  $p \approx C_{B^-} = 6 \times 10^{19} \text{ cm}^{-3}$

$$C_{B_3I} = \frac{C_B^{\text{total}} - C_{B^-}}{3} = \frac{10^{20} - 6 \times 10^{19}}{3} = 1.33 \times 10^{19} \text{ cm}^{-3}$$

$$\Delta G_{\text{binding}} = kT \ln \left( \frac{(1.33 \times 10^{19} \text{ cm}^{-3})(5 \times 10^{22} \text{ cm}^{-3})^3}{(6 \times 10^{19} \text{ cm}^{-3})^3 (4.8 \times 10^{10} \text{ cm}^{-3}) \left(\frac{6 \times 10^{19} \text{ cm}^{-3}}{3.2 \times 10^{18} \text{ cm}^{-3}}\right)^3} \right)$$

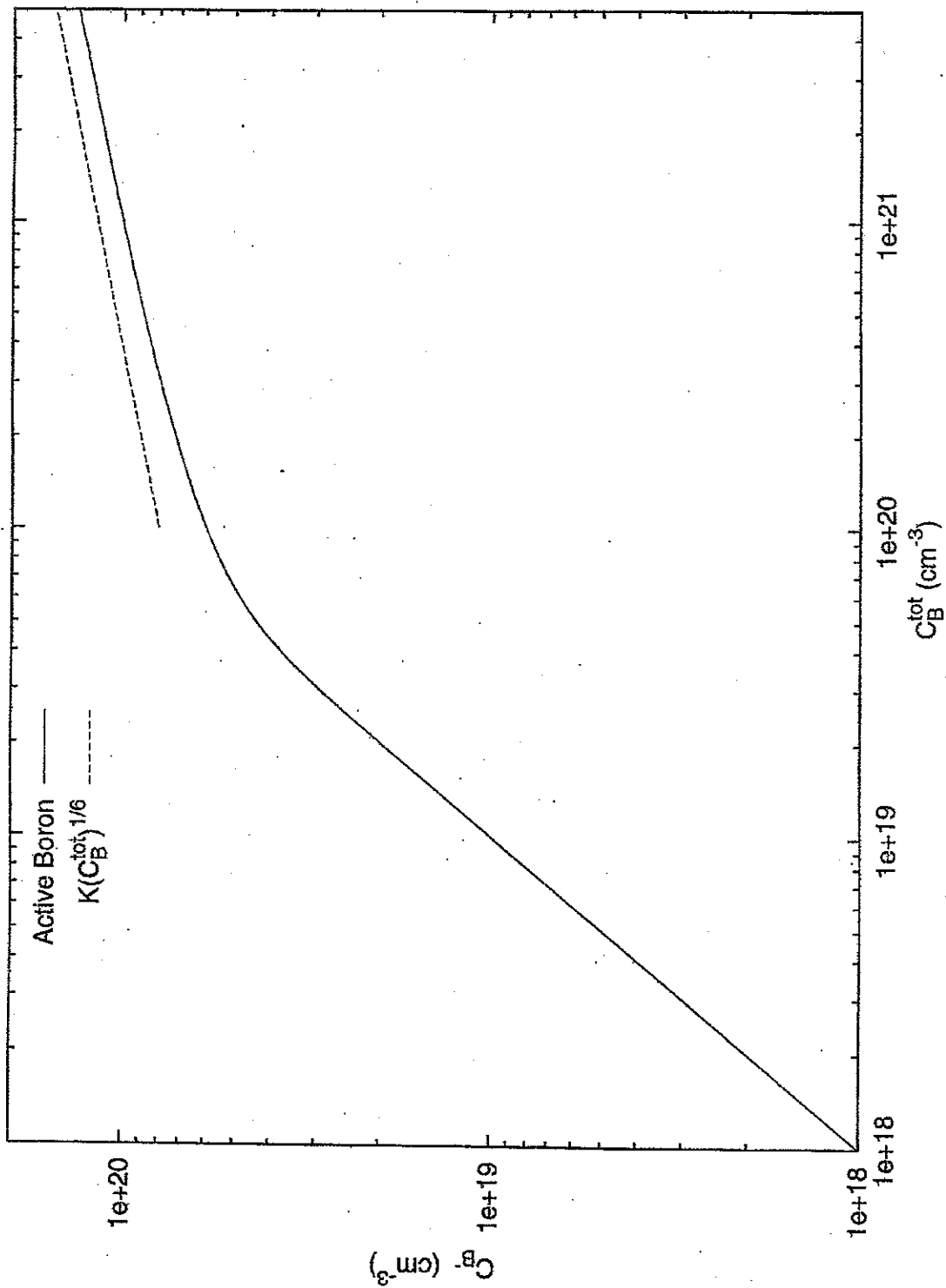
$$= 3.12 \text{ eV} \Rightarrow K = 2.0 \times 10^{-55} \text{ cm}^9$$

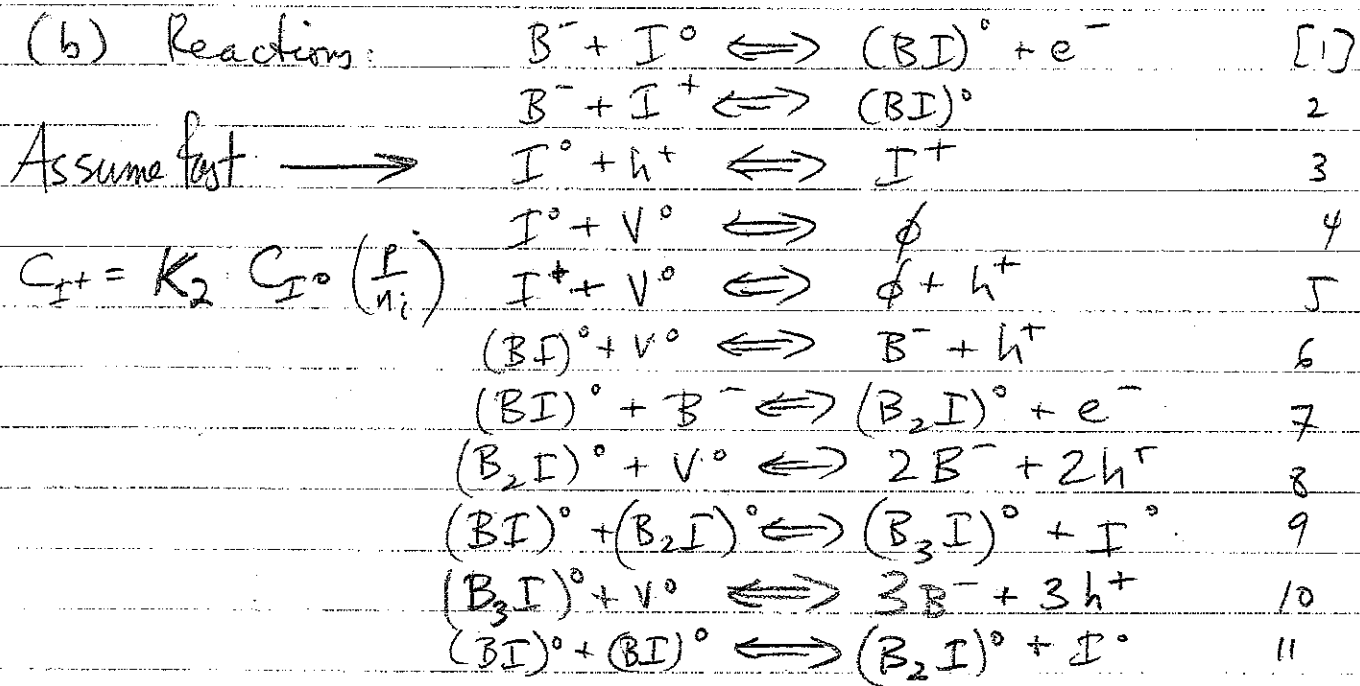
If we define  $\Delta G_{\text{binding}}$  relative to hole (or electron) energy in system with  $p = 6 \times 10^{19} \text{ cm}^{-3}$ , we leave off  $(p/n_i)^3$  factor so

$$\Delta G_{\text{binding}} = 4.01 \text{ eV (shifted by } 3 * (E_{f_i} - E_f))$$

$$P = \frac{C_{B^-}}{2} + \sqrt{\left(\frac{C_{B^-}}{2}\right)^2 + n_i^2}$$

$$C^{\text{total}} \approx C_{B^-} + 3C_{B_3I} = C_{B^-} + 3K(C_{B^-})^3 \left(\frac{p}{n_i}\right)^3$$





$$(A) \quad \frac{\partial C_{B^-}}{\partial t} = -R_1 - R_2 + R_6 - R_7 + 2R_8 + 3R_{10}$$

$$(B) \quad \frac{\partial (C_{I^0} + C_{I^+})}{\partial t} = -R_1 - R_2 - R_4 - R_5 + R_9 + R_{11} - \nabla \cdot (F_{I^0} + F_{I^+})$$

$$(C) \quad \frac{\partial C_{V^0}}{\partial t} = -R_4 - R_5 - R_6 - R_8 - R_{10} - \nabla \cdot F_{V^0}$$

$$(D) \quad \frac{\partial C_{(BI)^0}}{\partial t} = R_1 + R_2 - R_6 - R_7 - R_9 - 2R_{11} - \nabla \cdot F_{(BI)^0}$$

$$(E) \quad \frac{\partial C_{(B_2I)^0}}{\partial t} = R_7 - R_8 - R_9 + R_{11}$$

$$(F) \quad \frac{\partial C_{(B_3I)^0}}{\partial t} = R_9 - R_{10}$$

Note:  $K_1 = K_3 K_2$

Assume  $B^- + I^0 \rightleftharpoons (BI)^0 + e^-$  is fast  $C_{(BI)^0} = K_1 C_{B^-} C_{I^0} \left(\frac{P}{n_i}\right)$

Replace (A), (B) & D w/ this algebraic equation and (A)+(D), (B)+(D)

$$(A') \quad \frac{\partial (C_B^- + C_{(BI)}^{\circ})}{\partial t} = -2R_7 + 2R_8 + 3R_{10} - R_9 - 2R_{11} - \nabla \cdot \vec{F}_{(BI)}^{\circ}$$

$$(B') \quad \frac{\partial (C_I^{\circ} + C_{I^-} + C_{(BI)}^{\circ})}{\partial t} = -R_4 - R_5 - R_6 - R_7 - R_{11}$$

(c) Now assume reaction 7 is fast,  $C_{(B_2I)}^{\circ} = K_7 C_{(BI)}^{\circ} C_B^- \left(\frac{P}{n_i}\right)$

Replace  $A', B'$  &  $E$  w/  $A'+2E$  and  $B'+E$

$$= K_{(BI)}^{\circ} C_B^- C_I^{\circ} \left(\frac{P}{n_i}\right)^2$$

where  $K_{(B_2I)}^{\circ} = K_1 K_7$

$$(A'') \quad \frac{\partial (C_B^- + \cancel{C_{(BI)}^{\circ}} + \cancel{C_{(B_2I)}^{\circ}})}{\partial t} = +3R_{10} - 3R_9 - \nabla \cdot \vec{F}_{(BI)}^{\circ}$$

$$(B'') \quad \frac{\partial (C_I^{\circ} + C_{I^-} + C_{(BI)}^{\circ} + C_{(B_2I)}^{\circ})}{\partial t} = -R_4 - R_5 - R_6 - R_8 - R_9 - \nabla \cdot (F_{I^{\circ}} + F_{I^-} + F_{(BI)}^{\circ})$$

Plus (c) and (f)

(d)  $R_9$  is rate-limiting process for  $B_3I$  formation, so  $R_{10}$  can be neglected in comparison

$$\begin{aligned} R_9 &= k_9^f \left[ C_{(BI)}^{\circ} C_{(B_2I)}^{\circ} - C_{(B_3I)}^{\circ} C_I^{\circ} / K_9 \right] \\ &= k_9^f \left[ K_1 C_B^- C_I^{\circ} \left(\frac{P}{n_i}\right) K_1 K_7 C_B^- C_I^{\circ} \left(\frac{P}{n_i}\right)^2 - \frac{C_{(B_3I)}^{\circ} C_I^{\circ}}{K_9} \right] \\ &= k_9^f K_1^2 K_7 C_I^{\circ} \left[ C_B^-^3 C_I^{\circ} \left(\frac{P}{n_i}\right)^3 - \frac{C_{(B_3I)}^{\circ}}{K_{(B_3I)}^{\circ}} \right] \end{aligned}$$

where  $K_{(B_3I)}^{\circ} = K_9 K_1^2 K_7$

If  $B_2I^\circ$  and  $BI^-$  react readily to form  $B_3I^\circ$  plus  $I^\circ$ , then  $k$  can be estimated

as  $4\pi a (D_{B_2I^\circ} + D_{BI^-}) = 4\pi a D_{(BI)^-}$ , with  $a \sim 5\text{\AA}$  (capture radius)

$$(d) \quad C_{B_3I^\circ} = K_{B_3I^\circ} (C_{B^-})^3 C_{I^\circ} \left(\frac{p}{n_i}\right)^3$$

where  $K_{B_3I^\circ} = K_1^2 K_7 K_9$  as defined on previous page.

Combine to eliminate  $R_{(B_3I)^\circ} = R_9$

$$A''' = A'' + 3F \quad \frac{\partial (C_{B^-} + C_{B_2I^\circ} + 2C_{B_2I^\circ} + 3C_{B_3I^\circ})}{\partial t} = -\nabla \cdot F_{(BI)^\circ} \quad (\text{total B})$$

$$B''' = B'' + F \quad \frac{\partial (C_{I^\circ} + C_{I^\circ} + C_{(BI)^\circ} + C_{(B_2I)^\circ} + C_{(B_3I)^\circ})}{\partial t} = -\nabla \cdot (F_{I^\circ} + F_{I^\circ} + F_{(BI)^\circ}) - R_{I/V} \quad (\text{total I})$$

$$C \quad \frac{\partial C_{V^\circ}}{\partial t} = -\nabla \cdot J_{V^\circ} - R_{I/V} \quad (\text{total V})$$

plus  $C_{(BI)^\circ} = K_1 \left(\frac{p}{n_i}\right) C_{B^-} C_{I^\circ}$ ,  $C_{(B_2I)^\circ} = \underbrace{K_1^2 K_7}_{K_{(B_2I)^\circ}} C_{B^-}^2 C_{I^\circ} \left(\frac{p}{n_i}\right)^2$

where  $R_{I/V} = R_4 + R_5 + R_6 + R_8 + R_{10}$

$$3. \Delta H^{\ddagger} = -0.9 \text{ eV}, \Delta S^{\ddagger} = 10^{-4} \text{ eV/K}, \sigma_p = 5 \times 10^7 \text{ eV/cm}$$

$$\Omega = \Omega_{\text{site}} = 2 \times 10^{-23} \text{ cm}^3 = 1/C_s$$

$$(a) C_A^{ss} = C_s \exp\left(-\frac{\Delta S^{\ddagger}}{k}\right) \exp\left(\frac{\Delta H^{\ddagger}}{kT}\right) \\ = 2.14 \times 10^{18} \text{ cm}^{-3}$$

$$(b) \Delta G_n = n \Delta G_n^{\infty} + P_n \sigma_p \quad \Delta G_n^{\infty} = -kT \ln\left(\frac{C_A}{C_A^{ss}}\right)$$

For a disk,  $P_n = 2\pi r$ ,  $V_n = \pi r^2 h = n\Omega$   
( $h = 0.27 \text{ nm} = \text{thickness}$ )

$$r = \sqrt{\frac{n\Omega}{\pi h}}, \text{ so } P_n = 2\sqrt{\frac{n\pi\Omega}{h}}$$

critical size defined by  $\left. \frac{d\Delta G_n}{dn} \right|_{n_c} = 0$

$$\left. \frac{d\Delta G_n}{dn} \right|_{n_c} = -kT \ln\left(\frac{C_A}{C_A^{ss}}\right) + 2\sqrt{\frac{\pi\Omega}{h}} \frac{1}{2} n_c^{-1/2} \sigma_p = 0$$

$$n_c = \frac{\pi\Omega\sigma_p^2}{h(kT \ln(C_A/C_A^{ss}))^2}$$

$$(c) \Delta G_{n_c} = -n_c kT \ln\left(\frac{C_A}{C_A^{ss}}\right) + 2\sigma_p \sqrt{\frac{n_c \pi \Omega}{h}}$$

$$\text{For } C_A/C_A^{ss} = 100, \quad n_c = 26.9 (27), \quad \Delta G_{n_c} = 12.5 \text{ eV}$$

$$= 10^4, \quad n_c = 6.73 (7), \quad \Delta G_{n_c} = 6.25 \text{ eV}$$

$$= 10 \quad n_c = 107.6 (108) \quad \Delta G_{n_c} = -25.0 \text{ eV}$$